

Renewable Power Generation by Solar Particle Receiver Driven Sulphur Storage Cycle

SO₃ splitting catalytic systems development

Dr. George Karagiannakis

Principal Researcher at the Chemical Process & Energy Resources Institute / Centre for Research & Technology Hellas (CPERI/CERTH)



The reaction – background information & challenges

The Solid Sulphur Cycle

	Reaction	Temperature
Sulphuric acid decomposition	$2\text{H}_2\text{SO}_4(\text{aq}) \rightarrow 2\text{H}_2\text{O}(\text{g}) + 2\text{SO}_3(\text{g})$ $2\text{SO}_3(\text{g}) \rightarrow \text{O}_2(\text{g}) + 2\text{SO}_2(\text{g})$	450-500°C 700-950°C
Disproportionation	$2\text{H}_2\text{O}(\text{l}) + 3\text{SO}_2(\text{g}) \rightarrow 2\text{H}_2\text{SO}_4(\text{aq}) + \text{S}(\text{s})$	50-200°C
Sulphur Combustion	$\text{S}(\text{l}) + \text{O}_2(\text{g}) \rightarrow \text{SO}_2(\text{g})$	500-1500°C



Common for all sulfur-based thermochemical cycles

Catalyst	Temperature	Performance	Conclusion
Pt/Al ₂ O ₃ (TiO ₂)	700-800°C	Activity close to thermodynamic, Pt sublimation, sulfidation	Not currently considered
Fe ₂ O ₃	800-900°C	Fair but lower activity cf. best performers, stable long-term	Benchmark catalyst, low cost
Cr ₂ O ₃	800-900°C	High activity, Cr leaching	Not currently considered
Fe _x Cr _{1-x} O ₃	800-900°C	High activity, eventual Cr leaching, structural changes	Not currently considered
CuO	800-900°C	High activity, structural changes	Cost issue
CuO/Al ₂ O ₃	800-900°C	High activity, stable long-term	Promising, minimize Cu content
Cu-Fe-Al mixed ox.	800-900°C	High activity, structural changes / not sufficiently tested	Likely not preferred option
Cu _{1-x} V _x O _z	600-650°C	High activity but with dilute SO ₃ , stable, partial liquefaction	Promising but challenging

Main challenge: *Chemically & thermally harsh conditions for catalysts & reactor construction materials*

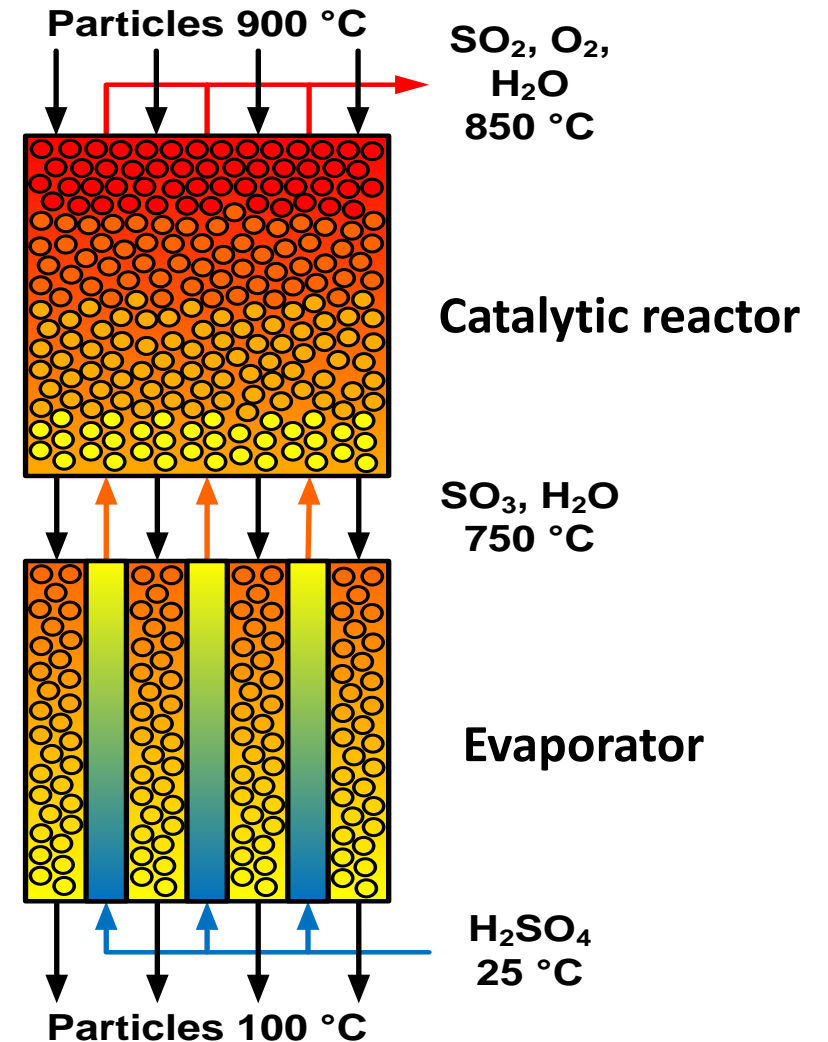
The PEGASUS approach – straightforward concept (I)

Catalytically-modified particles (proppants) as **both HTF & catalyst** for SO_3 splitting

Reactor downstream the particle receiver



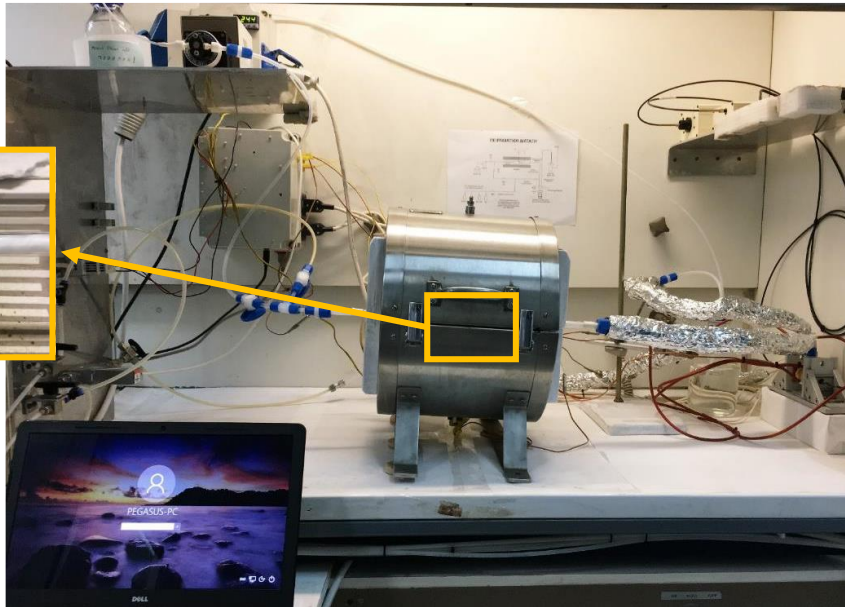
“Catalytic” Fe/Cu/Mn-modified bauxite proppants → moving catalyst bed → direct contact with SO_3 vapours ($\text{SO}_3 \rightarrow \text{SO}_2 + \text{O}_2$); downstream indirect evaporation of H_2SO_4 in SO_3 and $\text{H}_2\text{O}_{(g)}$ in a counter-flow cascade-like configuration.



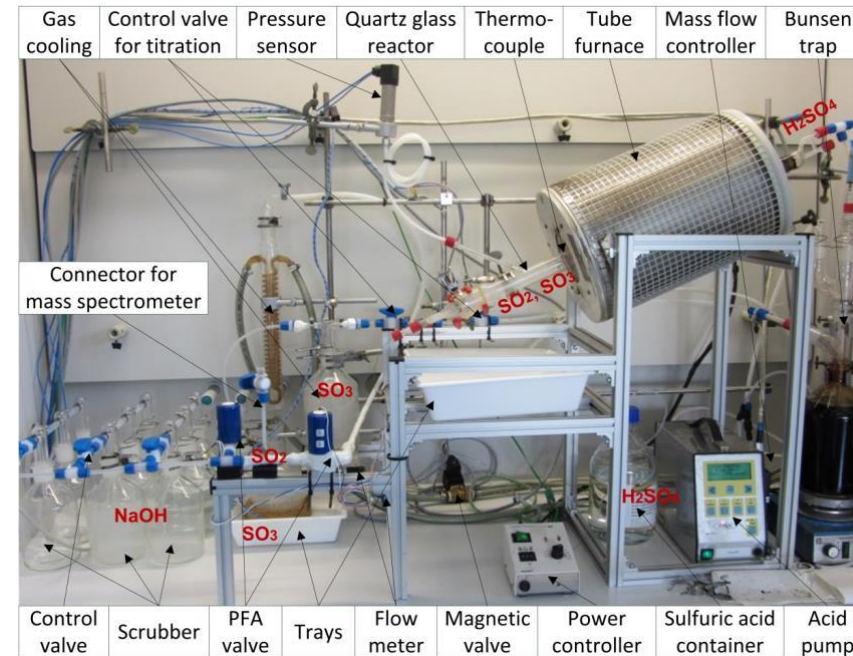
Catalytic evaluation of particles & proppants (II)

Catalytic & thermomechanical evaluation of > 60 samples:

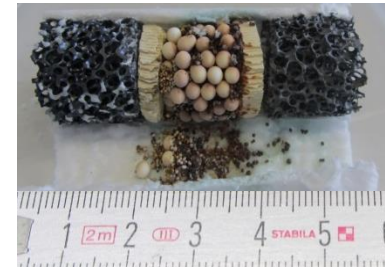
- ✓ *Modified & unmodified bauxite-based proppants*
- ✓ *Iron oxide-based dense particles*
- ✓ *Copper oxide-based dense particles*



Screening setup (1 – 10 h)



Long-term stability setup (100 - > 1000 h)

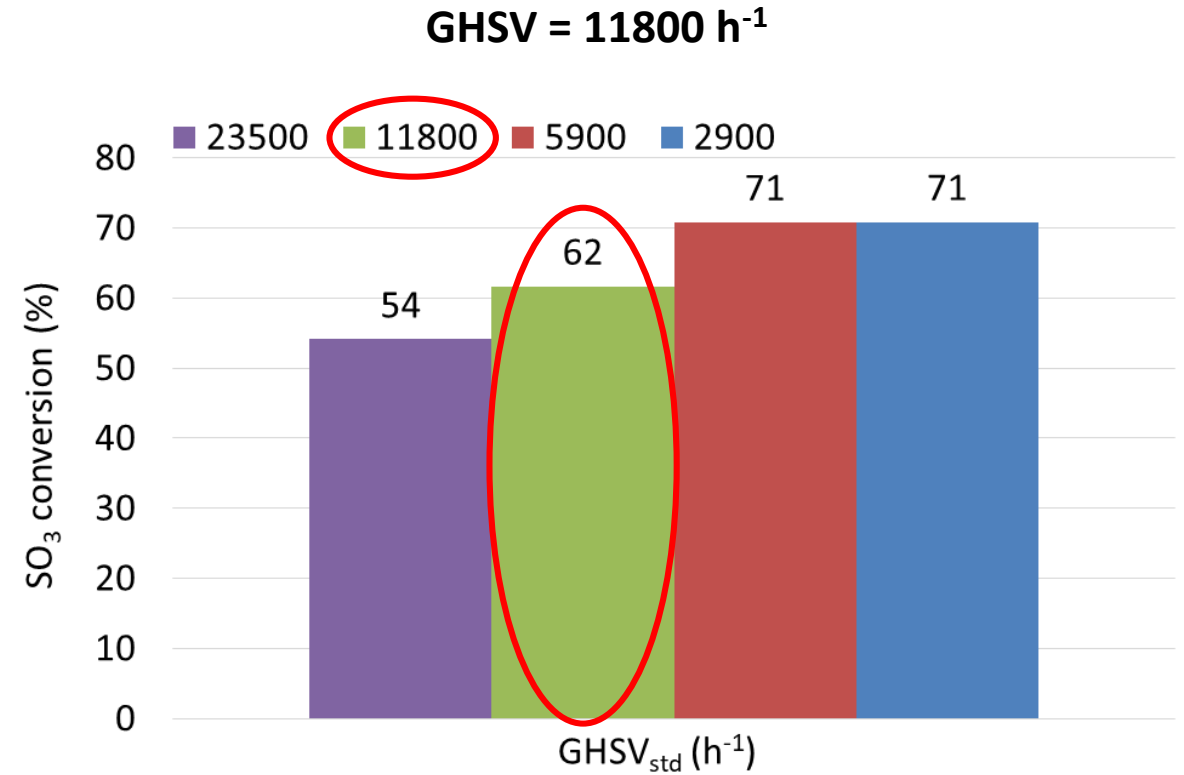
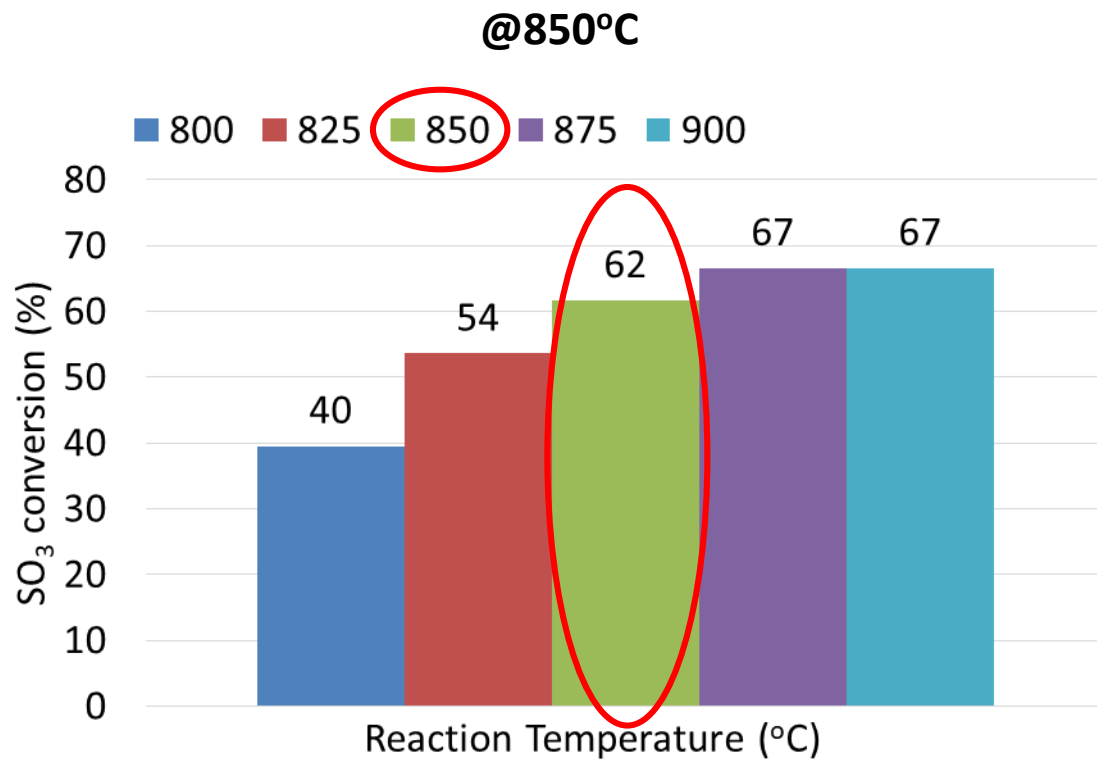


- Evaluation in fixed bed reactors with concentrated sulfuric acid feed @ 800-900°C
- Analysis by: SO₂ via UV-Vis spectrometry, O₂ measurements, titration

Catalytic evaluation of particles & proppants (III)

Parametric tests: effect of reaction temperature & residence time/GHSV on SO₃ conversion

Sample: Cu-Mn-O modified proppant



Catalytic evaluation of particles & proppants (IV)

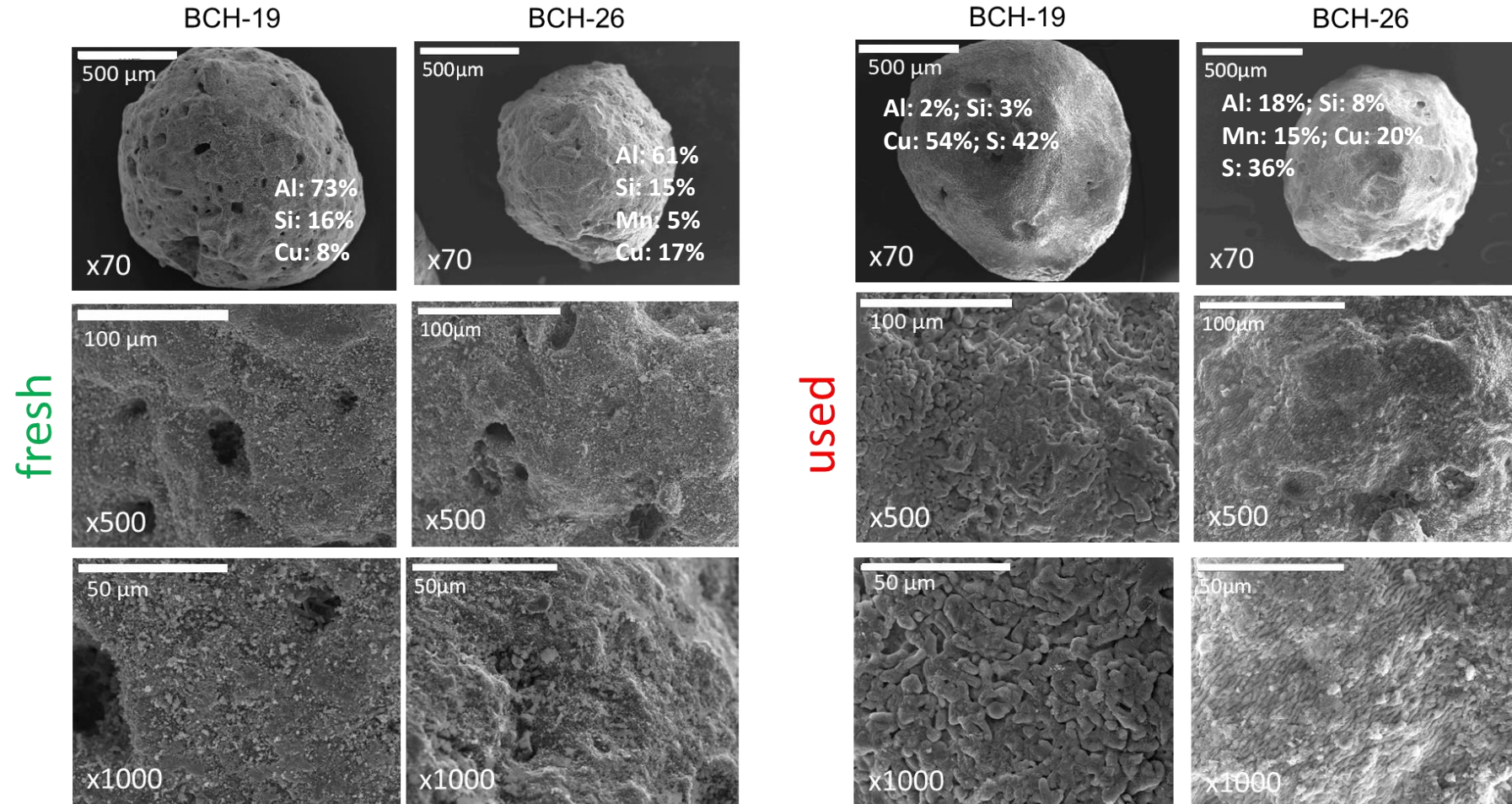
Most promising samples from screening studies - overview

No	Sample name	SO ₃ conversion (%) @850°C	Crushing Strength (in N)		CS % change
			Fresh particles	Used particles	
1	CuO_clay=15/85_1 dense particles	63.9	16	18	+12.5
2	CuO_clay=15/85_2 dense particles	63.4	15	22	+46.7
3	BCH-18 (Cu-modified proppants)	62.4	102	77	-24.5
4	BCH-25 (Cu-Mn-modified proppants)	61.6	55	57	+3.6
5	BCH-26 (Cu-Mn-modified proppants)	59.4	53	53	0
6	CuO_clay=75/25 dense particles	59.3	32	33	+3.1
7	BCH-19 (Cu-modified proppants)	59.3	74	69	-6.8
8	Fe ₂ O ₃ particles dense particles	54.8	23	29	+26.1

- Choice on the basis of combined high SO₃ conversion, thermomechanical stability (i.e. CS parameter) & in-principle production scalability
- Additional purpose-designed attrition tests indicated that thermomechanical stability still needs to be improved

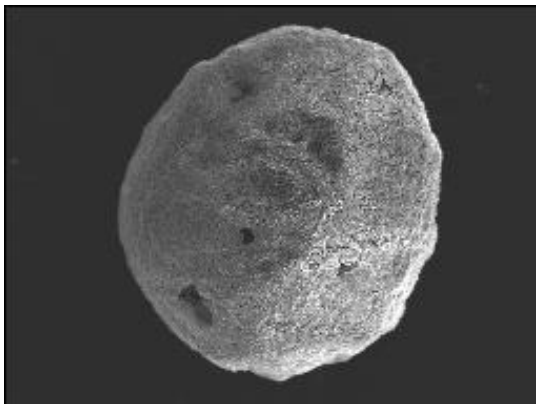
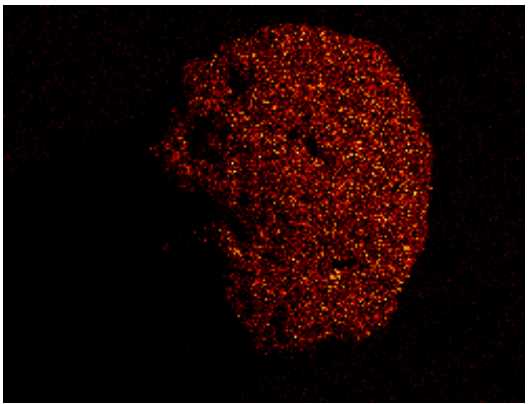
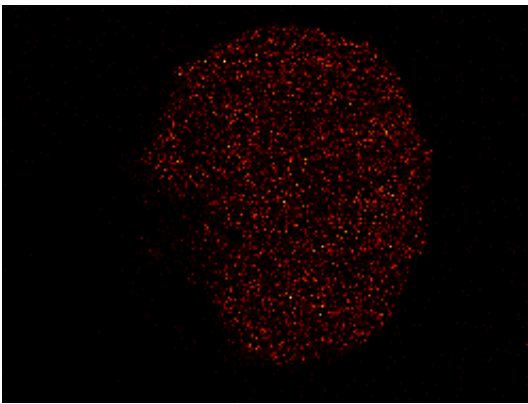
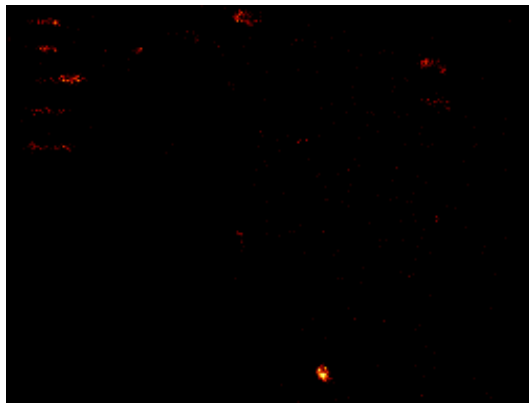
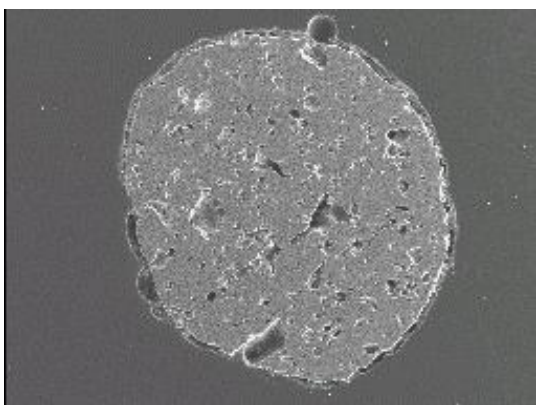
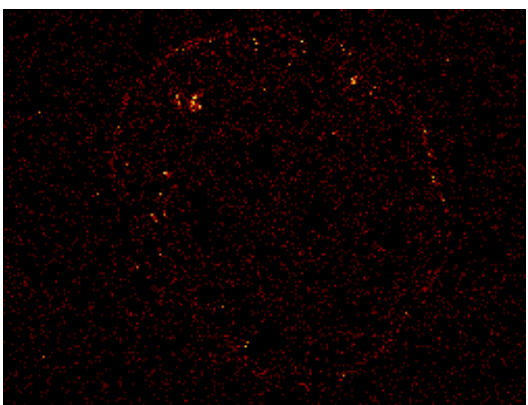
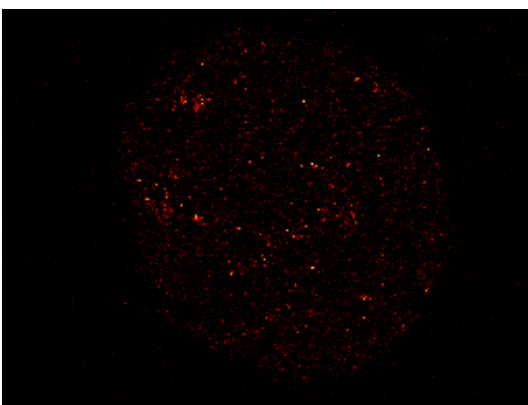
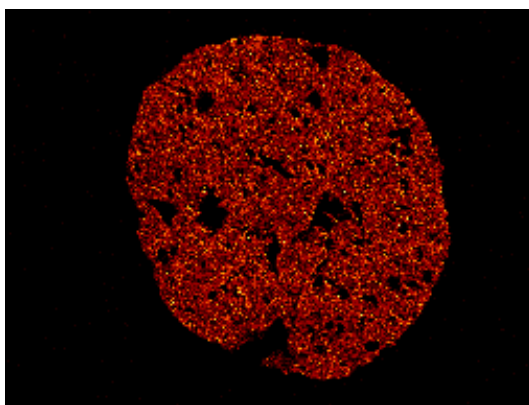
Post characterization of exposed samples – indicative results (I)

Comparative physicochemical characterization of pristine (fresh) & exposed (used) samples



- Macroporosity visible in the fresh/used samples. Signs of sintering in used samples
- Atomic analysis (wt%): Al, Si, Cu & Mn as main phases; S clearly detected in the used samples

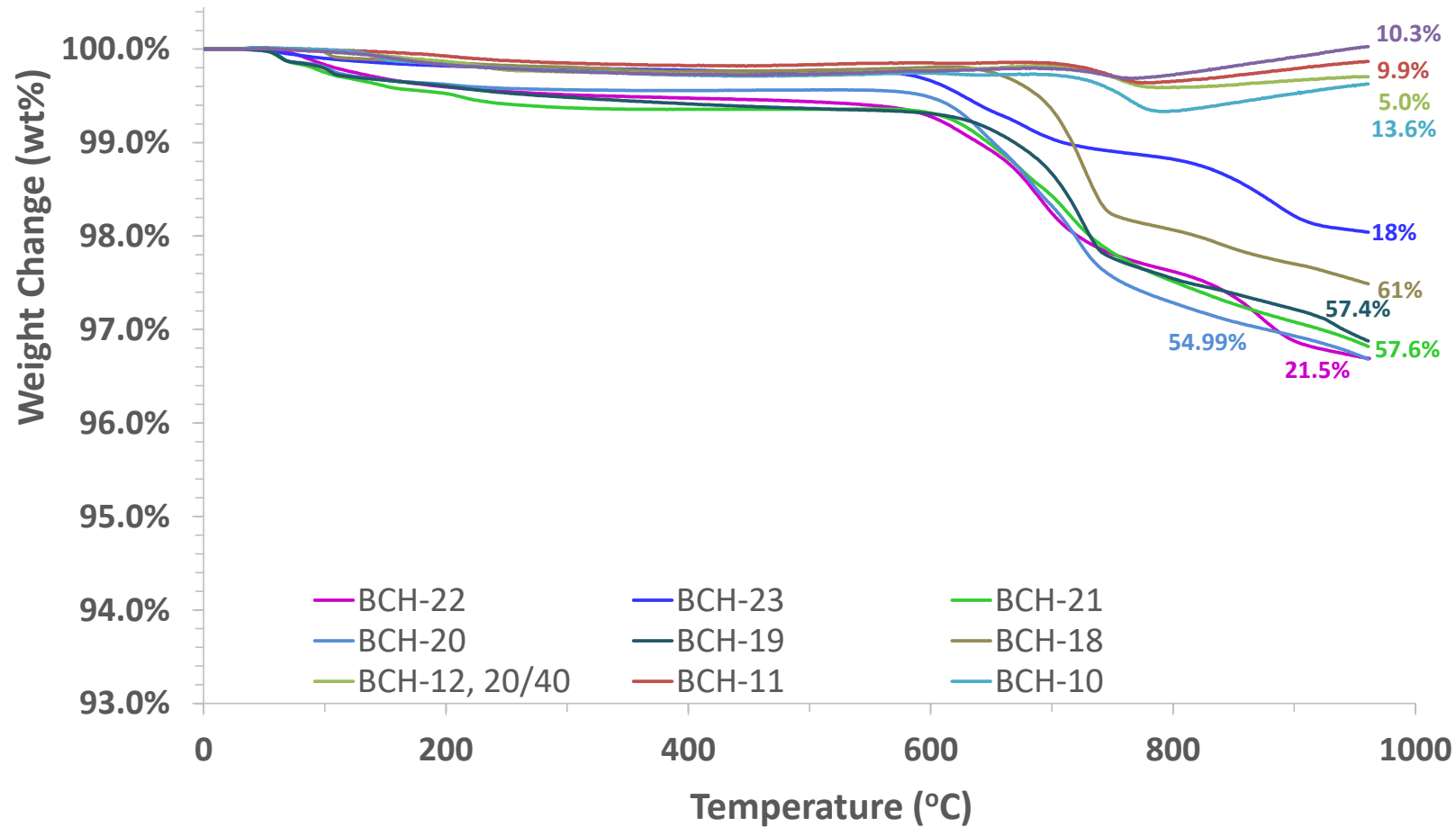
Post characterization of exposed samples – indicative results (II)

Sample view		Element		
		S	Cu	Al
Surface				
Cross-section				

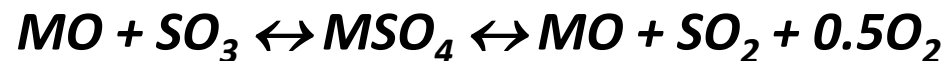


- Strong indication for the formation of a surface CuO-rich layer
- Sulfur detected mostly on the surface (spatial correlation with CuO)

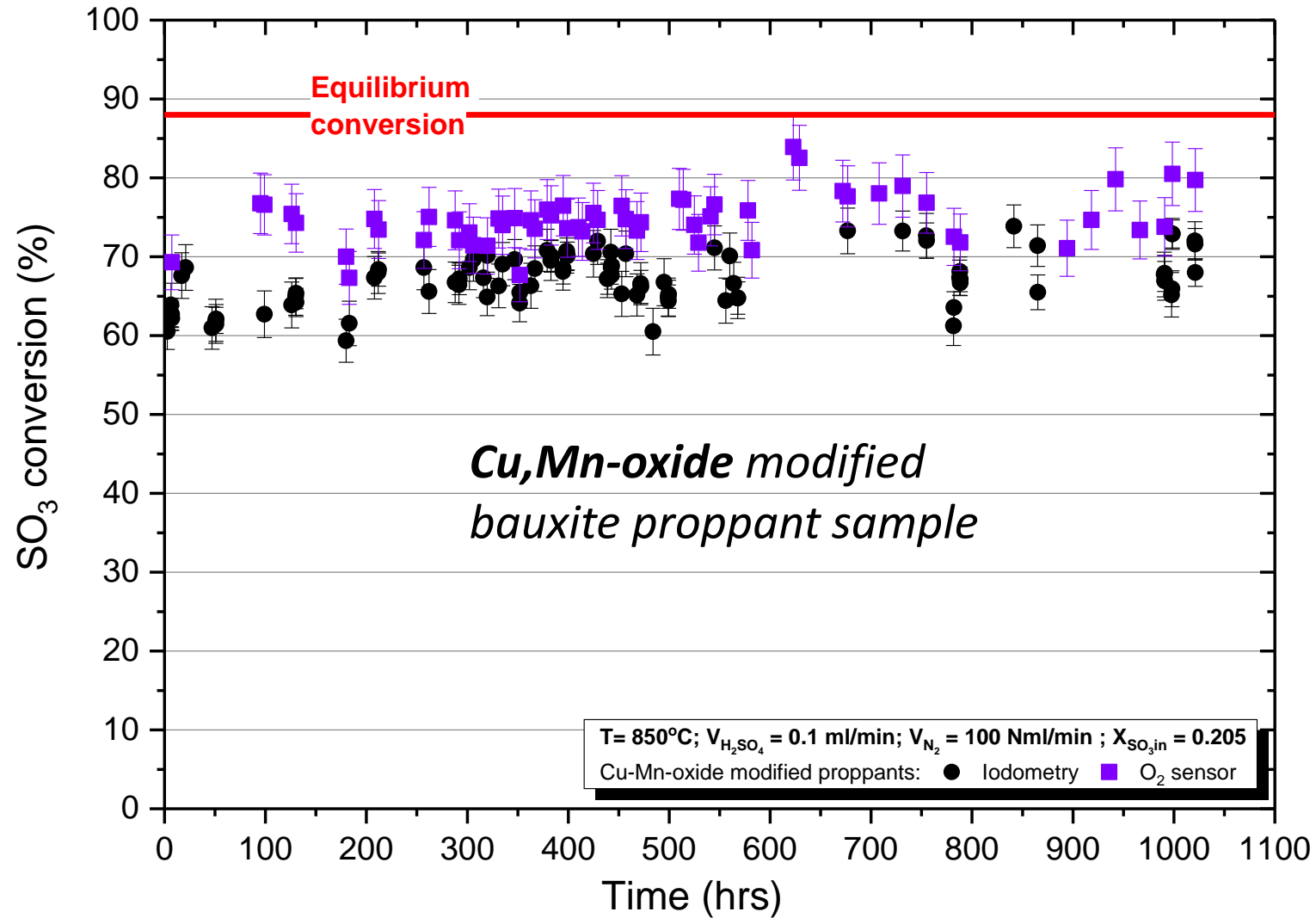
Post characterization of exposed samples – indicative results (III)



- Weight loss due to sulphates decomposition is directly proportional to catalytic activity
- Reaction mechanism via cyclic sulphates formation & decomposition:



Long-term exposure test of best performing modified proppants



- High & stable conversion @ 60-80% (equilibrium conversion @ conditions employed ~ 89 %)
- No performance loss after > 1000 h on stream

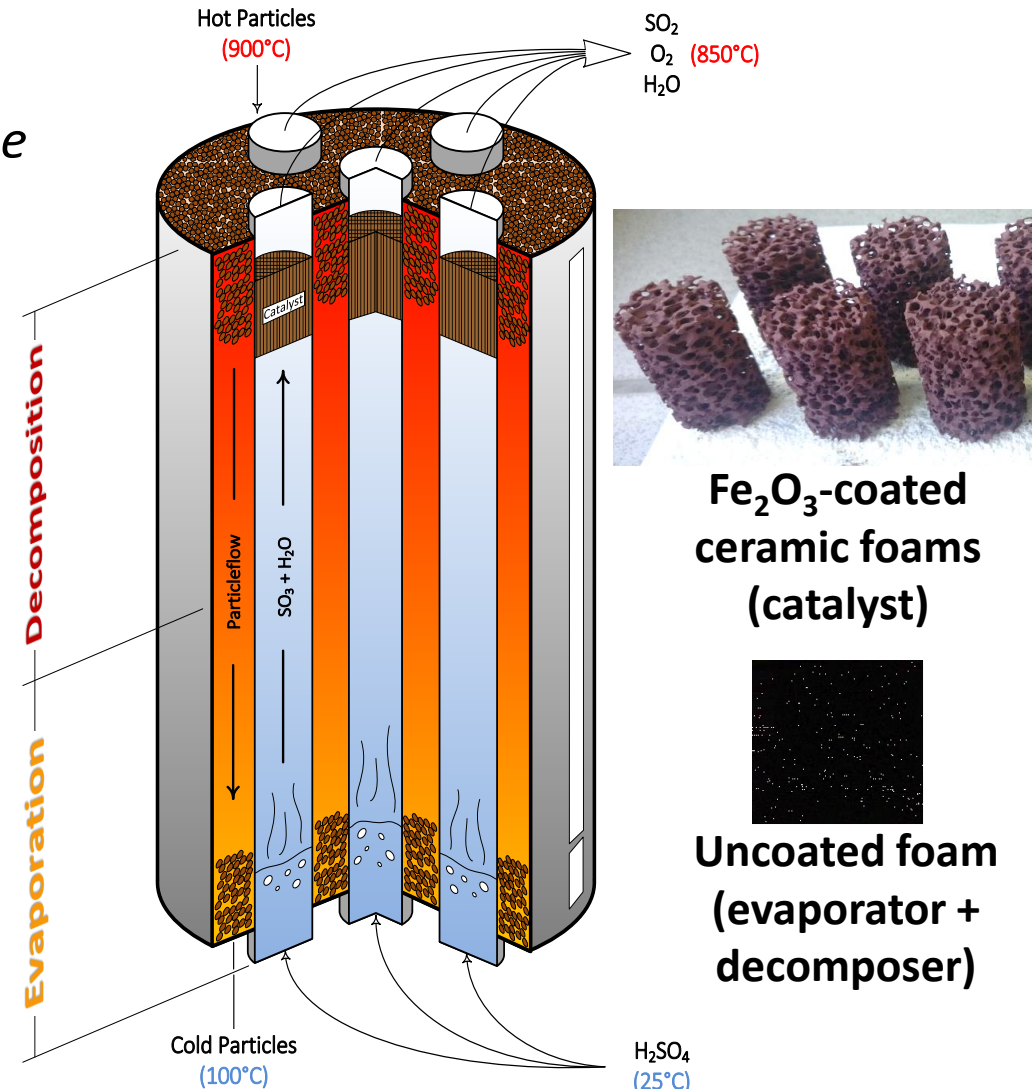
The PEGASUS approach – revised concept

Challenges of straightforward concept:

- ✓ *Catalytic modified proppants: costly, complicated production & of low thermomechanical stability*
- ✓ *Directly exposed particles likely to cause corrosion to the receiver (due to residual sulphates)*

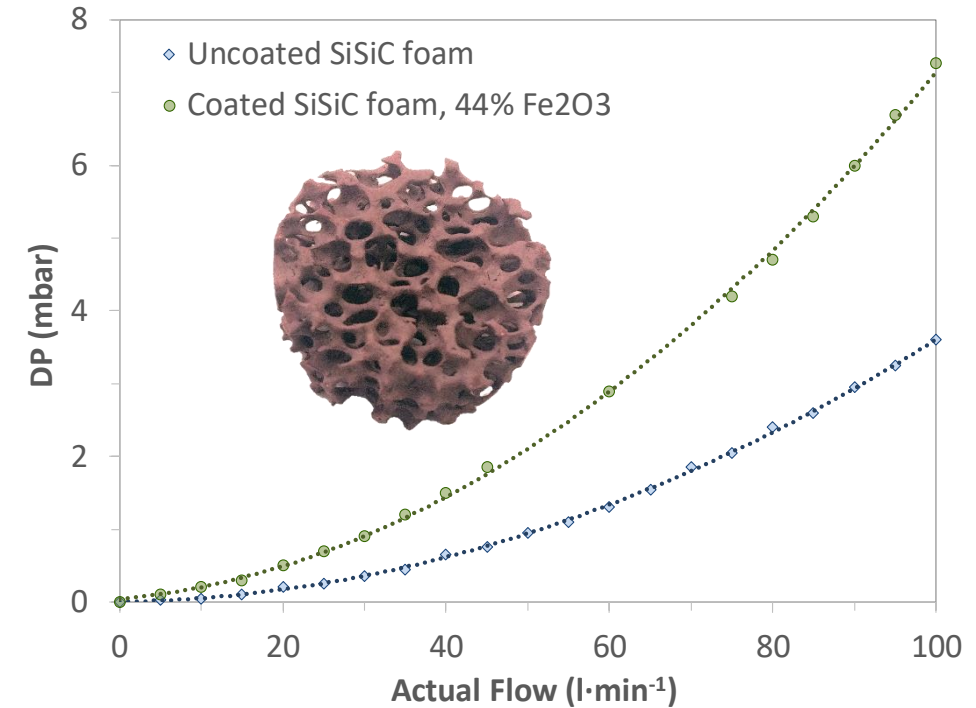
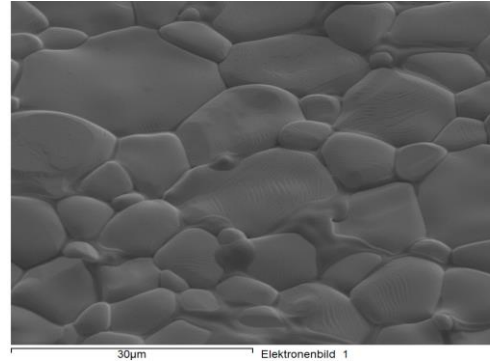
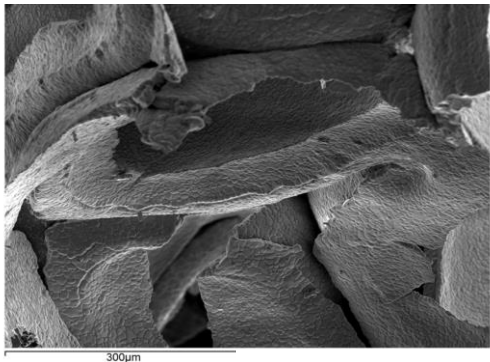
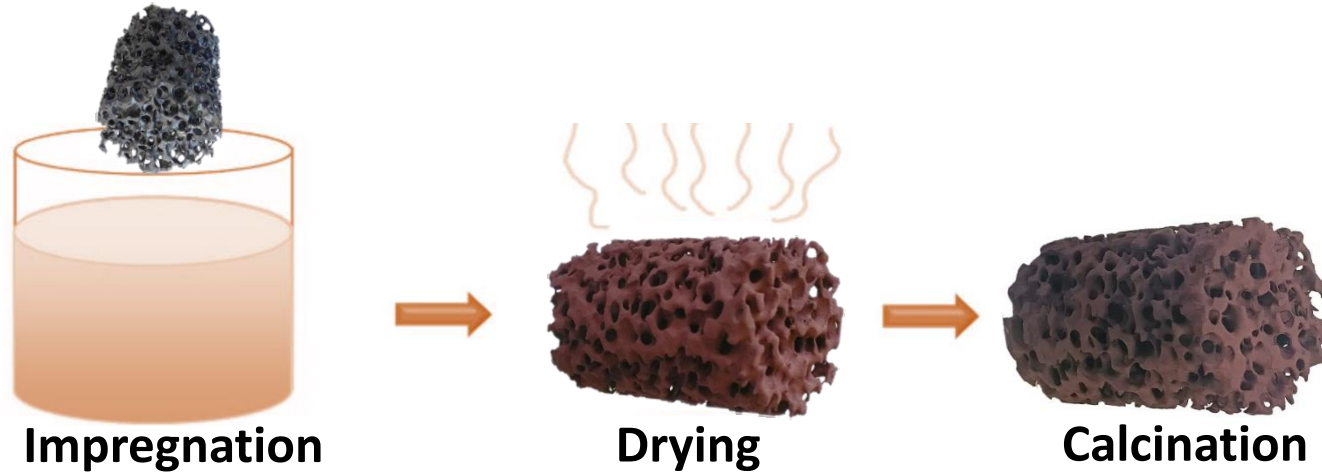
Non-catalytic, cheap, “plain” bauxite proppants → shell-and-tube sulphuric acid evaporator/SO₃ splitting reactor cascade → **indirect heat transfer** between the particles on the shell-side and fluid (H₂SO₄ vapours) on the tube-side, which therein will come into contact with a **non-moving catalyst bed**.

Concept adopted in the project for experimental validation → tbd in the next presentation



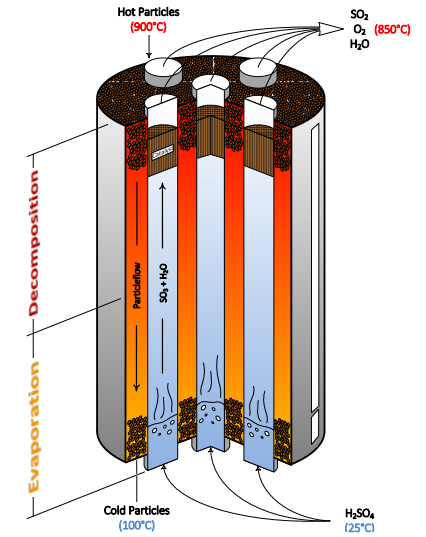
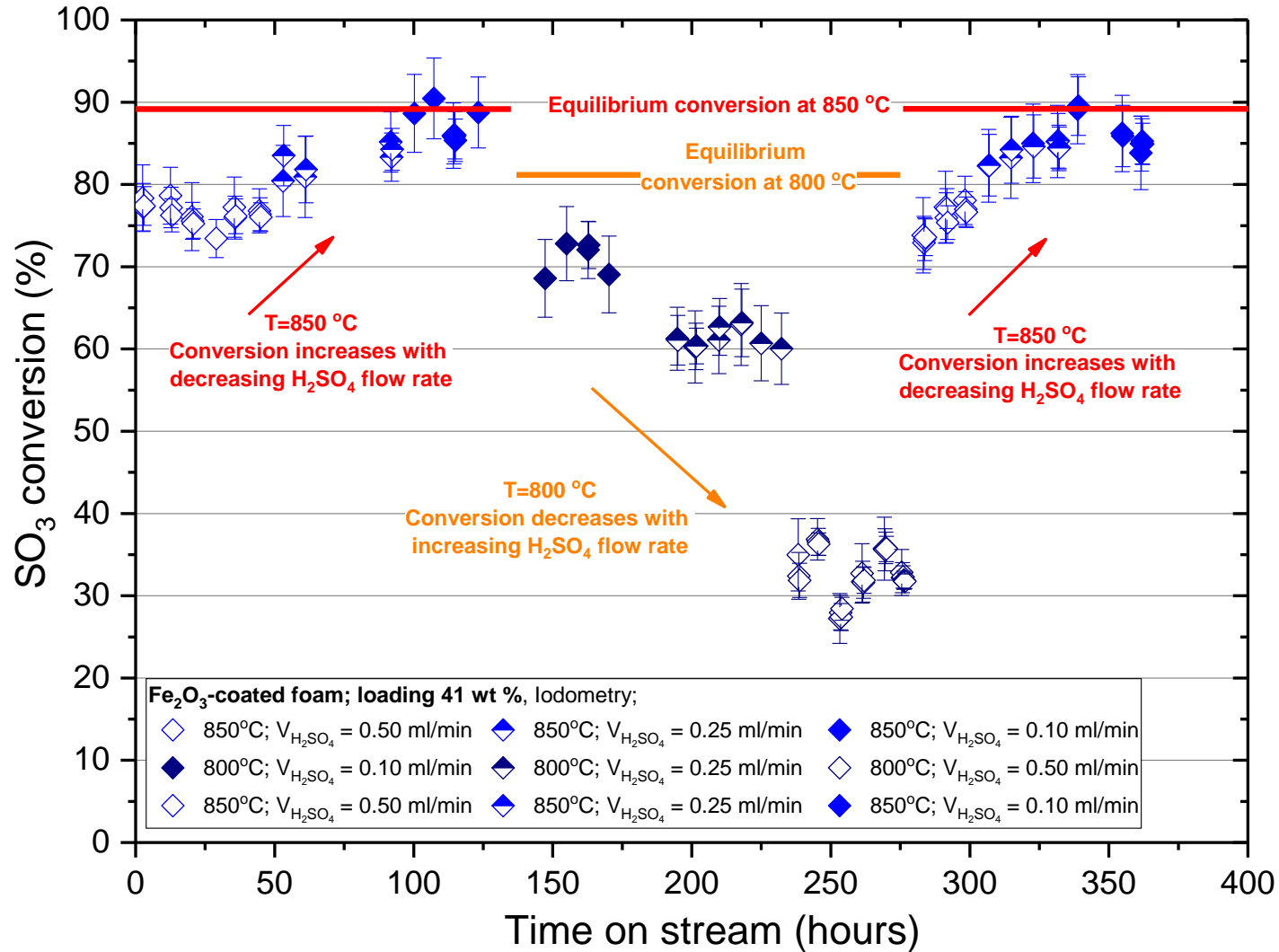
The PEGASUS revised concept – preparation of catalytic structures

Slurry/dip coating of SiSiC foams \rightarrow Fe_2O_3



- Coating of 24 segments of $\varnothing 24$ mm x 40 mm in total \rightarrow decomposer setup @DLR
- Average loading (Fe_2O_3 mass/clean foam mass): 37.5 wt%
- Homogeneous coating & low pressure drop of coated segments

Long-term exposure of a Fe₂O₃-coated foam



- Parametric experiments with same specimen, accumulating 362 h on-stream in total
- Near-equilibrium conversion @ 850°C within a range of H₂SO₄ flow rates & reproducible

Conclusions & future recommendations

- Modified proppants manufacturing to **combine high SO₃ splitting catalytic activity and HTF possible but far from optimized**:
 - ✓ *w.r.t. expected real operational environment → receiver's corrosion risk is high*
 - ✓ *Scaling-up feasibility → modified proppants manufacturing complicated & costly*
- Long term exposure (up to > 1000 h) under ideal lab-scale conditions → promising results
- Focus on the **indirect heat transfer concept** by using cheap proppants & catalytically active structures of high gas-solid contact area
 - ✓ *Careful design and room for optimization to achieve **efficient solid-solid heat transfer***
- Work to achieve validation under more realistic conditions & for long-term operation
- Development of a next version of decomposer reaction **@ high pressure** (P > 10 bar)



Thank you for your attention!

www.pegasus-project.eu



Dr. George Karagiannakis

gkarag@certh.gr



Co-funded by the Horizon 2020
Framework Programme of the
European Union